

PAVLYUCHENKO, M.M.; KNYSH, V.L.

Determination of flotation activity from the angle of dip  
of air bubbles. Dokl. AN BSSR 8 no.6:390-393 1964. (MIRA 17:10)

1. Institut obshchey i neorganicheskoy khimii AN BSSR.

KNYSHCH, P.V., inzh.

Development of new pulverisation equipment at the Chernovtsy Plant (brief  
news. Energomashinostroenie 4 no.9:46 8 '58. (MIRA 11:11)  
(Chernovtsy--Milling machinery)

KAGAN, Ya.M.; KAMALOV, R.R.; ANTROPOV, A.D.; KNYSHENKO, G.N.

Density of the gas oil mixture in the annular space of wells  
equipped with sinking centrifugal pumps. Nefteprom. delo  
no.8:14-17 '64. (MIRA 17:12)

1. TSekh nauchno-issledovatel'skikh i proizvodstvennykh rabot  
neftepromyslovogo upravleniya "Aksakovneft".

MINOR, S. S. 1940, N. S. 1940, S. S. 1940, S. S. 1940.

1. List of wells equipped with pumps for underground well  
No. 111. Ref. no. 111-111. (111-111)

2. List of wells equipped with pumps for underground well  
No. 112. Ref. no. 112-112. (112-112)

I 21656-66 EST(m)/KPF(n)-2/EXP(t) IRE(h) JD/JQ  
ACC NR: AR6011594 SOURCE CODE: UR/0137/65/000/012/V031/V031

AUTHOR: Knyshov, E. A.; Konev, A. F.; Rubinshteyn, Ye. A.

ORG: none

TITLE: Optimum conditions for melting ferroniobium from commercial niobium pentoxide

SOURCE: Ref. zh. Metallurgiya, Abs. 127228

REF SOURCE: Sb. tr. Klyuchevsk. z-da ferrosplavov, vyp. 1, 1965, 69-73

TOPIC TAGS: niobium alloy, iron alloy, niobium compound, metal melting, slag, metal extraction

TRANSLATION: The authors studied the effects which the quantity of reducing agent in the charge as well as the slag and metal composition have on the technical and economic indices of aluminothermic Fe-Nb melting. It is found that maximum Nb extraction (85%) is reached when Al fed to the charge is 110% of the theoretically required amount. Lime was added to the charge in quantities up to 60% of the  $Nb_2O_5$  to study the effect of slag composition. Maximum Nb extraction (89.2%) was reached with the addition of lime to the charge in quantities of 25-30% of the  $Nb_2O_5$ . A further increase in lime concentration lowers the specific heat of the process and reduces the extraction of Nb. Maximum extraction of Nb into the ingot (96%) was observed with the addition of Fe ore to the charge

Cord 1/2

UDC: 669.168.001

ACC NR. AR6011594

in quantities of 20-30% of the  $Nb_2O_5$ . The resultant data are used for working out technical conditions for production of low-silicon Fe-Nb from commercial  $Nb_2O_5$ . D. Kashayeva. [VPRd]

SUB CODE: 11, 13 / SUBM DATE: none

Card 2/2

STASYUKOV, M.; CHUBAROV, P.; ZAYCHENKO, I., ratsionalizator; HUTSINSKIY, V.;  
VOLOVIK, A.; KNYSEV, I.; SHTEYNGART, M.

Why are the suggestions of Dnepropetrovsk metal workers ~~so slowly~~  
realized? Izobr. i rats. no. 11:24-25 M '58. (MIRA 11:12)

1. Dnepropetrovskiy metallurgicheskiy zavod im. Petrovskogo (for all  
except Shteyngart). 2. Starshiy inzh. Byuro izobreteley i  
ratsionalizatorov zavoda (for Stasyukov). 3. Zamestitel' predsedatelya  
zavodskogo komiteta (for Chubarov). 4. Zamestitel' sekretarya partynogo  
komiteta zavoda (for Hutsinskiy). 5. Zamestitel' sekretarya komiteta Leninskogo  
kommunisticheskogo soyusa molodshi Ukrainy (for Volovik). 6. Sotrudnik  
gazety "Tribuna metallurga" (for Knysev). 7. Spetsial'nyy korrespondent  
zhurnala "Izobretatel' i ratsionalizator" (for Shteyngart).  
(Dnepropetrovsk--Efficiency, Industrial)

ACC NR: AF6035928

SOURCE CODE: UR/0413/66/000/020/0194/0194

AUTHOR: Arinushkin, L. S., Dumov, V. I./ Knyshev, V. A. / Moskovskiy, V. D./ Polinovskiy, A. Yu./ Sharov, Yu. A.

ORG: none

TITLE: Pump unit for two-circuit fuel systems for power plants

SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no.20, 1966, 194

TOPIC TAGS: pump, <sup>engine</sup> fuel system, ~~two-circuit fuel system~~, fuel feed system, <sup>engine fuel pump</sup>

ABSTRACT: The proposed pump unit consists of a pump with a low pressure circuit and a pump with a high pressure circuit. To improve its efficiency and to decrease the system's size and weight, the impellers of both pumps are mounted on a common shaft and an annular collector is positioned between the impellers; the collector is connected by ducts to the low pressure pump outlet duct and to the high pressure pump inlet cavity. In order to improve the anticavitation characteristics of the unit, a variation of this unit is made so that the fuel by-pass from the high pressure circuit runs through a duct which is positioned tangentially to an annular chamber located at the unit inlet. (see Fig.1).

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annular chamber; 10- unit inlet

Orig. art. has: 1 figure.

[WA-88]

SUB CODE: 21/ SUB DATE: 005081001

CIA-RDP86-00513R000723410003-1"

Card 2/2



**KNYSHEV, Ya.**

For an early achievement of planned output. Mast. ugl. 4 no. 8:5  
A '55. (MIRA 8:10)

1. Brigadir navalootboyshchikov shakhty no. 21 imeni Khrushcheva  
tresta Sovetskugol' Stalinskoy oblasti  
(Donets Basin--Coal mines and mining)

L 1704-66 EMT(a)/EJA(d)/EMP(t)/EMP(k)/EMP(a)/EMP(b)/EMA(c) LIP(a) JU/EM  
 UR/0148/65/000/008/0073/0076  
 ACCESSION NR: AP5020978

AUTHOR: Polukhin, P. I.; Arkhangel'skiy, A. V.; Knyshev, Yu. V.; Masterov, V. A.

TITLE: Experimental study of the mechanics of rolling bimetal

SOURCE: IVUZ. Chernaya metallurgiya, no. 8, 1965, 73-79

TOPIC TAGS: bimetal, metal rolling, sheet metal, aluminum, copper, metal cladding

ABSTRACT: This study in the rolling of bimetal was conducted to provide information for selection of proper thicknesses of the initial metal sheets to give the required relative thickness in the final bimetal. The effect of the initial ratio of sheet thicknesses and the effect of total thickness on the strain and force parameters of the rolling process were examined using bimetal of aluminum A000 and electrolytic copper of equal thickness to make up sandwiches 2, 3, 5, 10, 15 and 20 mm thick, and using sandwiches in which the aluminum: copper thickness varied from 0.13 to 6.70. Deformation irregularities are reduced as the total thickness is reduced to 5 mm. The anomalous increase in irregularities below

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L 1704-66

ACCESSION NR: AP5020978

this thickness was attributed to the greater deformation of aluminum in comparison to copper as sheet thickness is reduced. The pressure of the rolls is greater on copper than on aluminum of equivalent thickness, and specific pressures are minimum on sandwiches about 10 mm thick. As the thickness of the copper sheet in a 10 mm sandwich is decreased its deformation is reduced, and when the aluminum: copper ratio reaches 5.2-6.7 the sheets do not laminate. The distribution of torque between the rolls for bimetal over 5 mm thick was examined, but further study is required for thinner bimetals. The forward slip on aluminum is always greater than on copper when rolling bimetal, and as the initial thickness is increased from 2 to 13 mm the slip on copper is reduced to zero. Measurements of the contact arc between the metal sheets and the rolls showed that its length is determined by sandwich thickness, the amount of reduction per pass, and the ratio of the mechanical properties of the sheets and their thicknesses. Because of the complexity of the effects associated with the deformation of bimetal, further study of the specific pressure and of friction force diagrams is required. Orig. art. has: 5 figures

Card 2/3

L 1704-66

ACCESSION NR: AP5020978

3

ASSOCIATION: Moskovskiy institut stali i splavov (Moscow Institute for Steels and Alloys)

44,55

SUBMITTED: 29Apr65

ENCL: 00

SUB CODE: MM

NR REF SOV: 002

OTHER: 000

*mlb*  
Card 3/3

L 20778-66 EWT(d)/EWT(m)/EWP(w)/EWP(v)/T/EWP(t)/EWP(k)/EWP(h)/EWP(l) IJF(e)

AUC NR: AP6003558 JD/HW/JH

SOURCE CODE: UR/0148/65/000/010/0080/0083

AUTHOR: Polukhin, P. I.; Arkhangel'skiy, A. V.; Knyazev, Yu. V.; Mastarov, V. A. 49-  
B

ORG: Moscow Institute of Steel and Alloys (Moskovskiy institut stali i splavov)

TITLE: Certain features of the rolling of bimetal strip 10

SOURCE: IVUZ. Chernaya metallurgiya, no. 10, 1965, 80-83

TOPIC TAGS: bimetal, metal rolling, aluminum, copper, yield strength, plastic deformation

ABSTRACT: Reduction in area during rolling was investigated for a 40 mm wide Al-Cu strip as a function of the initial mechanical properties of each metal (as modified by preliminary peening or annealing) and the rate of their strain hardening during rolling. Owing to preliminary peening the initial ratio between the yield points of Cu and Al,  $\sigma_{Cu}/\sigma_{Al}$ , was 0.8 (peened Al, Al, annealed Cu) and 17 (peened Cu, annealed Al). The distribution of total reduction in area between the layers of the strip, the total and mean unit pressure, the linear pressure per unit width of the strip, the distribution of pressure over the arc of contact with the roll and the length of that arc, and the torque on the rolls were investigated in a rolling mill with 27 27

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DOC: 621.771.23.01

L 20778-66

ACC NR: AP6005558

rolls of 170-mm diameter. It was found that, when rolling a strip with layers of a thickness ratio of 1:1, the mean unit pressure is sufficiently closely equal to the mean yield point of the strip; thus, the averaged yield point for both layers of the strip may be used for the approximate calculation of rolling stresses. Equality of torques on both rolls was observed for the case of a 45% reduction in area, when the mean radial pressures on Al and Cu differed, and when the corresponding linear pressures on the rolls also differed; this proves yet again the need to take into account the asymmetry of deformation of the strip. The length of the arc of contact with the roll also differed, being greater for the layer with the greater deformation resistance (Al). Orig. art. has: 5 figures.

SUB CODE: 11, 13/ SUM DATE: 20Jul65/ ORIG REF: 000/ OTH REF: 000

Card 2/2 ynb

PEVOMAYSKIY, G.S.; SIMONOV, A.K.; KRYSEVICH, N.A.

Field tests of new repellents against mosquitoes in a hot climate.  
Trudy Astr. zap. no.9:192-196 '64.

(MIRA 18:10)

**KNYSHOV, F.**

Methodological work with teachers and instructors. Prof.-tekh. obr.  
22 no.3:26-28 Mr '65. (MIRA 18:7)

1. Direktor uchebno-kursovogo kombinata tresta "Urupmed'stroy"  
Glavnogo upravleniya po stroitel'stvu v rayonakh Severnogo  
Kavkaza Ministerstva gorodskogo i sel'skogo stroitel'stva RS-SR.



14(5)

PHASE I BOOK EXPLOITATION

SOV/2400

Shamshov, F.A., N.P. Knyupfer, N.I. Nikolayev, S.N. Tarakanov, and Ye.A. Sal'ye

Razvedochnoye bureniye (Exploratory Drilling) Moscow, Gosgeoltekhizdat, 1958. 485 p. Errata slip inserted. 20,000 copies printed.

Ed. (Title page): F.A. Shamshov; Ed. (Inside book): V.A. Boravlev; Ed. of Publishing House: N.B. Nekrasova; Tech. Ed.: O.A. Oarova.

**PURPOSE:** This textbook is intended for petroleum geology and engineering students in schools of higher learning and for engineering personnel engaged in exploratory drilling.

**COVERAGE:** The book covers the main theoretical and practical aspects of exploratory drilling. Equipment and methods are described and their effectiveness evaluated. Data on oil drilling tools and auxiliary equipment include specifications and diagrams. N.P. Knyupfer prepared the chapter on measurement in directional drilling including the deflection of boreholes. N.I. Nikolayev contributed the data on rotary and turbo-drilling,

~~Card 1/2~~

<p><b>KNUPFER, N. P.</b></p>	
<p>5383. THERMOMETER (K - 47) FOR MEASURING TEMPERATURE OF ROCK IN MINE WORKINGS. Knupfer, N. P. and Krakowski, S. A. (Ugol (Coal), No. 1949, 29-30).</p>	<p>The authors, with the assistance of the Giprokhel-Institut at Leningrad have constructed an electric thermometer especially adapted to the measurement of rock temperature. The device consists of a copper thermometer and Wheatstone bridge. The thermometer is mounted in a protecting paper sheath treated with bakelite and fitted with a brass cap. The diameter of the sheath and of the cap is 30 m.m.; the cap has the form of a truncated cone (60° angle), 5 m.m. in diameter at the top, and the thickness of the walls of the cap is about 1 m.m., and that of the blunt extremity 3 m.m. A layer of paper provides electric insulation between cone and winding. The winding consists of an enamelled copper wire 0.05 m.m. in diameter wound in a single layer round a paper cone, the size of which is equal to the inner cone of the cap. By means of an inner thread the cap is screwed to the bakelite pipe. On the other end of the pipe is a brass muff; into the latter is screwed an aluminium pipe, to which three or four similar pipes may be added consecutively, giving a total length of 3 m. The thermometer is introduced into hole of 2.5 m. length. Round the paper cone are</p>
<p>5383.5 METALLURGICAL LITERATURE CLASSIFICATION</p>	<p>14-00000</p>
<p>14-00000</p>	<p>14-00000</p>

wound more than 1 m. of copper wire, of resistance 118 ohms at 16°C. The active arm is connected with the bridge by means of a twin-core cable of 4 m. length; the section of each core is 0.75 m.m.<sup>2</sup>. The whole equipment is carried in a wooden case. The instrument is a three-range one; the precision of reading is ± 0.20. Current is supplied by two dry cells, which do not need replacement more often than 2 - 3 times per year. Tests showed the instrument to be suitable for measurement of temperatures between -4.6°C. and +85.5°C. (L)

M.C.B.

Knyšlitz, L.

11. 12. 13.

10/11/2007 10:11:11 AM

**1**

The President for Promoting Organization Development for High Schools  
Selected by the Association of Presidents

PERSONAL MAIL: 1960, No. 3, pp. 817-831

[illegible][illegible]

that in humans. In the specific kind of the present discovery the nitrogen compound, called the nucleoside was obtained in a best condition containing a specific kind of GTP called *the energy*. Based on the fact, results a promising method for producing high-energy, anti-oncogenes, especially for cells 1, 5-10.5 nitrogen compound can be obtained with GTP nucleoside. In the case with a specific kind of GTP-GTP, enzyme 2-6-1, 5 nitrogen compound will be obtained in a best way. In the energy and with a 10-12 kind of GTP nucleoside. There are 11 kinds of 11 kinds and 2 kinds nucleosides.

Page 35

IGNATENKO, G.F., insh.; FLINER, Yu.L., insh.; LAPPO, S.I., insh.; RUBINSHTEIN,  
Ye.A., insh.; KHYSHEV, E.A., insh.

Technology of making high-nitrogen, carbon-free, ferrochromium by  
the aluminothermic method. Stal' 20 no.9:817-818 S '60.

(MIRA 13:9)

1. Klyuchevskiy zavod ferrosplavov.

(Iron-chromium alloys—Metallurgy)

(Aluminothermy)

KNYSHEV, Ivan Nikitich; PRON', Vladimir Matveyevich; YURCHUK, V.I.,  
kand. ist. nauk, otv. red.; VALICOURA, V.A., red.; MATVIICHUK,  
A.A., tekhn. red.

[Our confident steps] Tverdoi postup'iu. Kiev, 1961. 45 p.  
(Obshchestvo po rasprostraneniю politicheskikh i nauchnykh  
znaniy Ukrainakoi SSR. Ser.1, no.20) (MIRA 15:2)  
(Dnepropetrovsk—Steel industry) (Efficiency, Industrial)

POLUKHIN, P.I.; GUN, O.Ya.; MASTEROV, V.A.; KNYSHEV, Yu.V.

Calculating forces and deformations in the reduction of laminated solids. Izv.vys.ucheb.sov.; Chern.met. 5 no.6:71-75 '62.

(MIRA 15:7)

1. Moskovskiy institut stali.  
(laminated metals) (Forging)

S/148/62/000/006/002/005  
E081/E435

AUTHORS: Polukhin, P.I., Gun, G.Ya., Masterov, V.A.,  
Knyshev, Yu.V.

TITLE: Calculation of the stresses and strains during the  
pressing of layered bodies

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Chernaya  
metallurgiya, no.6, 1962, 71-75

TEXT: The problem considered is the pressing out between dies of  
a material consisting of  $n$  layers of different substances (Fig.1)  
taking into account hardening, friction between the layers,  
and shear forces in the external zone. The work corresponding to  
the two latter effects is evaluated and, using the method of  
undetermined multipliers, formulae are derived which enable the  
specific pressure and the state of strain in the material to be  
calculated. A nomographic method of accomplishing the  
calculations is outlined. There are 2 figures.

ASSOCIATION: Moskovskiy institut stali (Moscow Steel Institute)

SUBMITTED: January 10, 1962

Card 1/2



KYSHOV, Ivan Nikitich; PRON', Vladimir Pavlovich; KESTERHIKO,  
P.P., red.

[Sprouts of the new, the communist way] Parostky novoho,  
komunistychnoho. Dnipropetrovs'k, Dnipropetrovs'ke knyzh-  
kove vyd-vo, 1961. 58 p.

(MIRA 17:10)

KNYSHOV, N.

Power workers master the trade. Prof.-tekh.obr. 12 no.12:8-9  
D '55. (MLA 9:3)  
(Electric engineering--Study and teaching)

KNYSHEVSKAYA, A. O.

"The use of radium and radioactive cobalt to treat cancerous formations on the eyelids." Min Health Ukrainian SSR. Khar'kov Medical Inst. Khar'kov, 1956. (Dissertations for the Degree of Candidate in Medical Science)

So: Knizhaya letopis', No. 16, 1956

KLEJMAN, Herman, agr ins.; KNYSZ, Jozef, agr ins.

9th International Electronics Congress in Rome, June 18-23, 1963.  
Przegl telekom 35 [i.e. 36] no.3:93-100 Mr '63.

1. Komitet do Spraw Techniki, Warszawa.

SOV/96-59-10-20/22

**AUTHORS:** Ko, A.P. (Dr.Tech.Sci.) and Kagan, Ya.A. (Cand.Tech.Sci.)

**TITLE:** Book Review - 'Standards for the Design and Calculation of Fuel-pulverising Installations'. Gosenergoizdat 1958. 159 pp.

**PERIODICAL:** Teploenergetika, 1959, Nr 10, pp 93-94 (USSR)

**ABSTRACT:** The material contained in this book is much needed by designers but it has not been very carefully drawn up and edited. More information is required about the design of large shaft mills.  
There are 1 table and 6 Soviet references.

Card 1/1

FODOR, Gyorgyne, dr.; KO, Klara

Device for processing signals from industrial measuring instruments using counting technique. Meres automat 12 no.4/5:134-139 '64.

1. Central Research Laboratory of Measuring Techniques.

V 1418\* - Comparison of the quality of centrifugal and stationary castings. Diagrams, photographs, tables, micrographs.  
H6 (Hungarian) Herbert Hartmann and  
János K. Orosz, v. 4, no. 10, Oct. 1955, p. 225-234.  
Comparative quality of centrifugal and stationary castings. Dia-  
grams, photographs, tables, micrographs.

of ①

KOALOV, I.G. (Physician; Cand Med Sci)

Dissertation: "Experiments for Using Skin from a Corpse in Otorhinolaryngology."

Second Moscow State Medical Institute imeni I.V. Stalin

23 May 49

SO Vecheryaya Moskva  
Sum 71



KOAYROVA, S.A., PHYSICIAN

CAND MED SCI

Dissertation: "Cardiotoxicity of the Human Serum in a Case of True Rheumatism."

23 May 49

Second Moscow State Medical Inst uncin

I.V. Stalin

SO Vecheryaya Morskva  
Sum 71

AYZENSHTEYN, M.D.; DEMIDOVICH, Ye.A.; KOBA, A.G.

Fluting inclined sections of roll grooves by disk knurling.  
Metallurg 9 no.5:34-35 My '64. (MIRA 17:8)

1. Yenakiyevskiy metallurgicheskiy zavod.

KOBA. G. [Koba, H.]

'Mechanized production of three-step ceramic blocks. Sil'. bud.  
10 no.9:17-18 s '60. (NIRA 13:6)

1. Predsedatel' Yavoriyskoy meshkolkhoznoy stroitel'noy organis-  
atsii L'vovskoy oblasti.  
(Building blocks)

USLONTSEV, B., KOBA, G. [Koba, H.]

Arched livestock buildings are being built by production-line methods.  
Sil', bud. 10 no.11:7-10-N '60. (MIRA 13:11)

1. Rukovoditel' gruppy sektora tekhnologii i organizatsii stroitel'stva  
Akademii stroitel'stva i arkhitektury USSR (for Uslontsev). 2. Ruko-  
voditel' soveta Yavorovskoy meshkol'khoznoy stroitel'noy organizatsii  
L'vovskoy oblasti (for Koba).

(Lvov Province--Farm buildings)  
(Collective farms--Interfarm cooperation)

KOBA, G. [Koba, H.]

Use of three-stepped blocks in rural construction. Bud. mat. i konstr.  
4 no.1:35-37 Ja-F '62. (MIRA 15:7)

1. Golova Yavorivs'kogo mishkolgospbuda.  
(Collective farms—Interfarm cooperation) (Ceramics)



15(2)

AUTHORS:

Yanpol'skaya, A. A., Koba, G. A.

SOV/131-59-3-5/18

TITLE:

Automatic Control of the Dosing of the Mass on the Press SM-143  
(Avtomaticheskoye regulirovaniye zasypki massy na presse SM-143)

PERIODICAL:

Ogneupory, 1959, Nr 3, PP 115-120 (USSR)

ABSTRACT:

On the press SM-143 the pressing effect is transformed by the press rods and the tensions forming in them are characteristic of this force. For measuring the tensions in the rods extensometers are used which are fastened to the opposed rod surfaces as can be seen from figure 1. The extensometers are connected by a non-equilibrium bridge which is fed by direct-current of constant voltage. The unbalance-voltage of the measuring bridge in its operation on an electron amplifier with a high input impedance can be computed from the formula  $U = 1.25 \frac{I}{2} \Delta R$ , where  $\Delta R$  denotes the variation of the bridge resistance,  $I$  the current strength of the bridge supply and 1.25 a constant. Figure 2 shows the simplified scheme of the automation-dosing of the mass and detailed descriptions are given next. Figure 3 gives the press curves. The scheme of the measuring bridge is shown on figure 4 and the basic scheme of the relay connecting block on figure 5. An experimental device was tried on a press SM-143

Card 1/2

Automatic Control of the Dosing of the Mass on the Press SM-143 SOV/131-59-3-5/18

of the Borovichakiy kombinat (Borovichi Kombinat). The tensions in the press rods, the current strength of the press electromotor and of the signals of the output relay were oscillographically recorded (Figs 6,7, and 8). At the same time the pressed products were examined as to weight and strength. Figure 9 shows the measuring and weighing results of the unworked press material with hand and automatic control of the mass dosing. By the automatic control of the mass dosing the uniformity of the products is increased and the work of the pressmen rendered more easy.- There are 9 figures and 6 references, 5 of which are Soviet.

ASSOCIATION: Vsesoyuznyy institut ogneporov (All-Union Institute for Refractories)

Card 2/2



KOBA, G.A., insh.

Device for a continuous removal of dust from a cyclone  
cone. Masl.-shir.prom. 28 no.7:41-42 JI '62. (MIRA 15:11)

1. Krasnodarskiy masloshirovoy kombinat imeni  
V.V. Kuybysheva.

(Separators (Machines))  
(Sunflower seed)

YAM, V.M., inzh.; KOBA, G.A.; GOLOSKOV, E.I.

Investigating stresses in frames of hydraulic press housings. Trudy  
Inst. ogneup. no.35:137-158 '63. (MIRA 17:12)

1. Vsesoyuznyy institut ogneuporov (for Koba). 2. Leningradskiy zavod  
"Metallist" (for Goloskov).

L 14008-66 FSS-2/ENT(1)/ENT(M)/ENP(1)/T/FCS(k) NW/JW/JND/OG/WE/RM

ACC NR: AP6004437

SOURCE CODE: UR/0414/65/000/003/0093/0098

AUTHOR: Dremin, A. N. (Moscow); Reznov, I. K. (Moscow); Koba, I. G. (Moscow) 52

ORG: none B

TITLE: Study of the reaction time in the detonation of liquid explosives by the electromagnetic method 21,44,55

SOURCE: Fizika goraniya i vzyryva, no. 3, 1965, 93-98

TOPIC TAGS: liquid explosive, detonation time

ABSTRACT: The reaction time  $\tau$  in the detonation of liquid explosives was studied by obtaining mass velocity profiles for charges of nitromethane and of a nitromethane-acetone mixture (75:25) using the previously described electromagnetic method (A. N. Dremin, K. K. Shvedov. PHTF, 1964, 2). To determine the effect of the size of the recording wire, which is located within the explosive charge in the electromagnetic method, the interaction of a detonation wave with a plate of aluminum foil (0.035 mm thick) and with a mica plate (0.04 mm thick) in nitromethane and nitromethane-acetone mixtures was studied using high-speed photography. It is shown that there is a detonation delay of about 0.15  $\mu$ sec behind both the aluminum and the mica plates. The mass velocity profiles recorded by the electromagnetic method with wires 0.035 and 0.22 mm thick for nitromethane and nitromethane-acetone mixtures also showed a detonation delay of about 0.17  $\mu$ sec in the case of the 0.035 mm wire, which is in good

Card 1/2

L 14008-66

ACC NR: AP6004437

agreement with the value obtained by the photographic measurements. With the 0.22 mm recording wire, the detonation delay was 0.45  $\mu$ sec. This difference is probably due to the difference in the intensities of the shock waves leaving the wires. The mass velocity in the shock wave behind the thin wire is greater than behind the thick wire. Thus, the recording wire creates a discontinuity dividing the combustion products and the unperturbed explosive. The mass velocity in the unperturbed explosive behind the shock wave may be calculated from the mass velocity of the combustion products and the shock adiabat of the explosive. The calculated value of the mass velocity behind the shock wave ( $u_1 = 1.86$  km/sec) is close to the value obtained from the electromagnetically recorded mass velocity profile ( $u_1 = 1.82$  km/sec). Extrapolated to the initial mass velocity recording point,  $u_1 = 2.04$  km/sec. The mass velocity sharply decreased from the initial maximum point to a certain break point after which the decrease became steady. The mass velocity at the break point was  $u_2 = 1.51$  km/sec. The time from the initial recording point to the sharp break point is the total reaction time  $\tau$ , and estimated to be equal to about 0.4 sec for the nitromethane-acetone mixture. The width of the reaction zone may be calculated when  $\tau$  is known:  $a = \tau(D - \bar{u})$ , where  $D$  is the detonation velocity and  $\bar{u}$  is the average mass velocity. For the nitromethane-acetone mixture (75:25),  $D = 5.75$  km/sec and  $\bar{u} = 1.77$  km/sec; thus  $a = 1.6$  mm. Orig. art. has: 4 figures and 1 formula. [PS]

SUB CODE: 19/ SUBM DATE: 02Feb65/ ORIG REF: 014/ OTH REF: 005/ ATD PRESS:

4196

Card 212 CC

KOBA, I.I., SHEVCHENKO, B.D., YARTSEV, P.A.

"High frequency system experiment placing "VP" in energy of 100 MEV."

Report submitted to the Intl. Conference on High Energy Physics and Nuclear  
Structure, Geneva, Switzerland. 25 Feb-2 Mar 1963

L 47312-05 EPA(w)-2/EAT(1)/EBC(t)/E/A(a)-2 PI-4/Ps-6 137(c) 17/08  
 6/0000/64/000/000/0293/0299

AUTHOR: Val'ter, A. K.; Grigor'yev, Yu. N.; Dudkina, I. N.; Ivanov, V. F.;  
 11'in, O. G.; Koba, I. I.; Kondratenko, V. V.; Mochevalkov, N. Y.; Tarasenko, A.  
 S.; Tarakhov, B. A.; Tolstoy, A. Ye.; Shenderovich, A. N.; Orlovsky, I. A.

TITLE: The apparatus of the Physicotechnical Institute, Academy of Sciences,  
 Ukrainian SSR, for colliding electron beams with energies of 200 x 100 Mev for ex-  
 periments on the scattering of electrons on electron

SOURCE: International Conference on High Energy Accelerators. Dubna, 1963.  
 Trudy. Moscow, Atomizdat, 1964, 293-299

TOPIC TAGS: high energy accelerator, high energy plasma, particle beam, particle  
 physics, charged particle beam

ABSTRACT: Work on colliding electron beams in the Physicotechnical Institute,  
 Academy of Sciences, Ukrainian SSR, was begun in 1960. The existence of linear  
 electron accelerators was basic for the initiation of such work. At the first  
 stage, it was decided to stop at electron storage devices of 100 Mev energy, since  
 it was found that even at such comparatively small energies of the colliding beams

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ACCESSION NR: AT5007922

many problems can be solved. The most convenient storage design is a system of race-tracks with a common linear section in which the collision of the two beams is effected. A distinctive property of the Institute's storage device is the great lengths of the linear sections, equal to 50 and 90 cm for a radius of revolution of 50 cm. The great length of one pair of linear sections in each of the rings was selected in order to provide for measurement of the minimum angle of scattering. Selection of a small radius of revolution was due to the requirement of minimum equilibrium dimensions of the beam and to the tendency to have a not too long time for damping of the beam oscillations. To localize the region of interaction, the beam orbits are distorted in the vertical plane by means of two "intersecting" magnets that create a homogeneous field in the radial direction. The magnets are arranged in the common linear section. The length of each of the "intersecting" magnets equals 10 cm, and the magnetic field strength is up to 640 oersteds. The magnets deflect the equilibrium orbit by 1 cm from the median plane. The quadrants have a constant magnetic field index of  $n = 0.425$ . The coupled magnets in the section that is common for both orbits have zero gradient; the index in the remaining sections is  $n_1 = 0.480$ . The stability of the Institute's system is characterized by a diagram showing field index  $n$  in the quadrants versus the field index  $n_1$  in the coupled magnets. The regions of stability and resonance lines of various

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orders are indicated in the diagram and discussed. The selected operating point is at a maximum distance from the resonances; in this case the frequencies of betatron radial and vertical (axial) oscillations are respectively equal to  $\nu_r = 1.145$ ,  $\nu_z = 0.6956$ . The internal dimensions of the vacuum chamber were  $100 \pm 40$  mm. The determining problem here was the conditions governing the beam input into the storage device. The beam is fed to an inflector through a magnetic channel. The initial conditions are so chosen that the beam can by-pass in the first six revolutions the inflector set a distance of 2.25 cm from the equilibrium orbit. The behavior of the storage device in the first six revolutions is described. In case the trailing edge of the magnetic field pulse lasts for three revolutions of the particles in the storage device, the introduction of particles into the chamber can also be prolonged in the course of three revolutions. In order to capture particles in the storage device it is necessary to create with the help of inflector magnets a magnetic field strength of  $H_1 = 1900$  oerstedes,  $H_{II} = 2630$  oerstedes. The system of tolerances is evaluated on the assumption of the following parameters for the input beam: width  $a = 0.5$  cm, height  $b = 0.3$  cm, angular divergence: radial  $\Delta\gamma_r = 2 \cdot 10^{-3}$  and vertical  $\Delta\gamma_z = 3 \cdot 10^{-4}$ . Preliminary measurements indicate that this data can be realized in the case of the Institute's apparatus. The requirements on

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the stability of the magnetic field of the inflector are:  $\Delta H_1/H_1 = 10\%$ ,  $\Delta H_{11}/H_{11} = 3\%$ . Taking into consideration the indicated quantities, the maximum values of the curvature of the radial betatron oscillations will be equal respectively to  $F_1 = 2.8$  cm,  $F_{11} = 4.1$  cm. According to computations, the equilibrium dimensions of the beam must be  $a_1 = 0.04$  cm;  $a_{11} = 0.2$  cm. Due to the quantum fluctuations in synchrotron radiation, the longitudinal dimension of the particle bunch equals 40 cm for a gap voltage of about 1.5 kilovolts. The mean energy expended on an electron per revolution, taking into account the coherent radiation, is equal to 220 electron-volts. The time of oscillation damping amounts to 100 msec. Alternate injection of the beam of electrons in the ring is effected by three sector magnets with double focusing. The introduction of a beam turned away from the accelerator and with zero initial conditions is ensured by the application of a cylindrical magnetic shield with a shielding coefficient varied along the length. All the magnets are supplied with power from sources that have a current stability of at least 0.02%. The report also discusses the vacuum chamber, voltage generator, and a few other aspects of the apparatus. Orig. art. has: 3 figures, 2 tables.

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L 47312-65

ACCESSION NR: AT8007922

ASSOCIATION: Fiziko-tekhnicheskii institut AN UkrSSR (Physicotechnical Institute,  
AN UkrSSR)

SUBMITTED: 26 May 84

ENCL: 00

SUB CODE: EE, RF

NO REF SOV: 000

OTHER: 000

Card 5/5714

SEMANCHUK, Dmitriy Iosifovich; KORA, M., redaktor; LEVCHENKO, O., tekhnichnyi redaktor

[Production capacities of industrial enterprises and methods for their efficient use] Vyrobnyshe potuzhnosti promyslovykh pidpryiemstv i shliakhy ikh ratsional'noho vykorystannia. Kyiv, Derzh.vyd-vo polit.lit-ry URSR, 1957. 46 p. (MLRA 10:10)  
(Russia--Industries)

CHUNTULOV, Vladimir Timofeyevich; KORA, M., red.; LAPCHENKO, K., tekhn. red.

[Ukrainian economy in full development] Roskvit ekonomiky Ukrainy'-  
koi SSR, Kyiv, Derzh. vyd-vo polit. lit-ry USSR, 1958. 64 p.  
(MIRA 1216)

(Ukraine--Economic conditions)

STUDENNIKOV, Timofey Vasil'yevich [Studenyykov, T.V.]; KOBA, M., red.;  
KOPITKOVA, N., tekhn. red.

[Transportation and communications in the Ukraine during the  
seven-year plan] Transport i sv'язok Ukrainy v Semyrihtsi.  
Kyiv, Derzh. vyd-vo polit. lit-ry URSR, 1960. 102 p.  
(MIRA 14:5)

(Ukraine--Communication and traffic)

OSTROVITYANOV, K.V.; GATOVSKIY, L.M. [Hatova's'kyi, L.M.]; KUZ'MINOV, I.I.;  
DUBOVENKO, Ye. [Dubovenko, I.E.], red.; KORA, M., red.; KOPITKOVA,  
M., tekhn.red.

[Political economy; textbook] Politychna ekonomia; pidruchnyk.  
Peraklad z 3 perer. i dop. rosiis'koho vyd. 1959 roku. Kyiv,  
Derzh.vyd-vo polit.lit-ry USSR, 1960. 686 p. (MIRA 13:7)

1. Akademiya nauk USSR, Kyiv, Institut ekonomiki,  
(Economics)

KARAKOZ, Ivan Ivanovich; KOBA, M., red.; MIL'KIN, Yu., tekhn. red.

[How to use the production funds of an enterprise to a better advantage] Shliakhy krasheho vykorystannia vyrobnych fondiv pidpryemstva. Kyiv, Derzh. vyd-vo polit. lit-ry URSR, 1961. 35 p.  
(MIRA 14:10)

(Industrial management)

RYZHKOV, Ivan Ivanovich, kand. ekonom. nauk, starshiy nauchnyy sotr.;  
KOBA, M., red.; GAVRILETS, D. [Havrylets', D.], tekhn. red.

[Production funds of industrial enterprises] Vyrobychi fondy promyslovykh pidpryemstv. Kyiv, Derzh. vyd-vo polit. lit-ry, USSR, 1961. 37 p. (MIRA 14:11)

1. Institut ekonomiki AN USSR (for Ryshkov).  
(Capital)



BONDARENKO, V.V., doktor ekon. nauk, otv. red.; KORA, M.F., red.;  
LISOVETS', O.M. [Lysovets', O.M.], tekhn. red.

[Problems of labor productivity statistics in industry and  
agriculture] Pytannia statystyky produktyvnosti pratsi v pro-  
myslovosti i sil's'komu hospodarstvi. Vyd-vo AN URSR, 1962.  
302 p. (MIRA 16:2)

1. Akademiya nauk URSR, Kiev. Instytut ekonomiky. 2. Zavedu-  
yushchiy otdelom statistiki Instituta ekonomiki Akademii nauk  
Ukr.SSR (for Bondarenko).

(Productivity accounting)

KOBA, M.F., red.; SERGEYEV, V.F. [Sergisev, V.F.], tekhn. red.

[The call of beacon lights] Malaky klyehut'; sbirnyk statei.  
Kyiv, Derzh. vyd-vo polit. lit-ry USSR, 1961. 120 p.

(MIRA 14:9)

(Agriculture--labor productivity)

KOBA, M.I. (Kiyev)

Connection between industrial training and the study of science in  
the secondary schools. Politekhn.obuch. no.3:20-22 Kr '59.

(MIRA 12:4)

(Science--Study and teaching)

KOBA, P.D., podpolkovnik meditsinskoy sluzhby

Sensitivity of the skin to ultraviolet rays in chronic gastritis  
and peptic ulcer. Voen.med.shir. no.3:86 '59. (MIRA 12:6)  
(ULTRAVIOLET RAYS--PHYSIOLOGICAL EFFECT) (STOMACH--DISEASES)  
(SKIN)

D JANKOWICZ, Jan; KOBIA, Stanislaw

Achievements of the Health Service in the Region of Kielce  
during 20 years of the Polish People's Republic. Wied. lek.  
18 no.21:Suppl.:1-3 19 8 ' 65.

KOBA, Stanisław; WESOŁOWSKI, Zenon

A case of agranulocytosis after pyranidone. Wiad. lek. 18  
no. 21:57-59 15 N ' 65.

1. Z Oddziału Zakaznego Szpitala Wojskowego w Kielcach  
(Ordynator: dr. med. S. Koba).

KOBA, Stanislaw

History of health service in the county in Kielce region  
in XIX century. Wlad. lek. 18 no.21:Suppl.:87-89  
15 N ' 65.

On certain infectious diseases in Kielce and in the  
county of Kielce i XIX century. Ibid.: Suppl.:91-95  
' 65.

28(1)

POL/46-4-1-8/15

AUTHOR:

Bayer, Ryzard, Chmielewski, Jerzy and Koba, Teresa

TITLE:

A 14 Channel Pulse Amplitude Analyzer with Counting Attachment (14-kanalowy analizator amplitudy z przystawka liczaca)

PERIODICAL:

Nukleonika, 1959, Vol 4, Nr 1, pp 87-91 (Poland)

ABSTRACT:

A description of the equipment with a block-diagram (Fig. 1) of the analyzer and the counting attachment is given. Furthermore the equipment is illustrated with and without the case. The range of application is outlined in brief. Analyzer - 14 channels; width of channel gate - 2,5,10 V; impulse amplitude - 16-171 V; width of impulse - 1-5 micr.; separation time - 2.5-5 micro-sec.; stability of discriminator -  $\pm 50$  mV; working conditions - 220 V, 900 VA; size - 570 x 360 x 2300 mm. Specification of counting attachment: scaling factor total count storage 999999; resolving time - numerator about 0.1 sec; size - 560 x 340 x 840 mm. There are 1 layout and 2 photographs.

Card 1/2



KOBA, V.G., Cand Tech Sci -- (diss) "Concerning the  
problem of the study of ~~shelling~~ <sup>shelling</sup> devices for the  
~~collecting the~~ <sup>collecting the</sup> seeds from the fruit of ~~the~~ <sup>drawings</sup>  
water melon." Saratov, 1958, 20 pp with sketches  
(Min of Agr USSR. Saratov Agr Inst) 150 copies  
(KL, 50-58, 125)

UL'YANOV, Aleksey Fedorovich, doktor tekhn. nauk; KOBA, Viktor  
Grigor'yevich, kand. tekhn. nauk; LOGVINOV, M., red.; BYKOVA, M.,  
red.; LUKASHEVICH, V., tekhn. red.

[Overall mechanization of livestock farms] Kompleksnaya mekha-  
nizatsiya v zhivotnovodstve. Saratov, Saratovskoe knizhnoe  
izd-vo, 1961. 261 p. (MIRA 15:4)

(Farm mechanization)

PARSHIN, Yu.A.; KOBA, V.I.; SAVENKO, A.L.

Remote safety device for placing the neutron source in the logging tool of the STP—NOD<sub>2</sub>—57 apparatus. Sbor.luch.rats.predl. pt. 2: 51-53 '63. (MIRA 17:5)

1. Glavnoye upravleniye geologii i okhrany nedr pri Sovetskiykh Ministroy BSSSR.

SOURCE: AN SSSR. Doklady, v. 154, no. 4, 1964, 894-896, and top half of insert  
ending page 894

L 22217-65

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hours at 200--800C. It was found that polyvinyl alcohol undergoes a change in molecular structure at 300C. The maximum concentration of aliphatic conjugated double bonds, minimum crystallinity, and maximum electric conductivity appear in the presence of inert gas at 300C. Pyrolysis at higher temperatures increases the rate of decomposition and lowers activation energy, apparently as a result of the "carbon structures" formed. The rate of decomposition was related to the increase in their surface area. The rate of decomposition increases in the presence of double bonds. The maximum resistivity and activation energy of the pyrolysis products is apparently associated with the complete breakdown of polyvinyl alcohol and disappearance of hydrogen bonding before any products are formed. Data are given in figures and tables.

ASSOCIATION: Vsesoyuznyy nauchno-issledovatel'skiy institut monokristallov, semiaktivatsionnykh materialov i esobu chistykh khimicheskikh veshchestv (All-Union Research Institute of Single Crystals, Semiconducting Materials, and High Purity Chemical Substances)

SUBMITTED: 26Sep63

ENCL: 00

SUB CODE: 00, 00

NO REF COPY: 005

OTHER: 005

100 1/2

GRYNBERG, M.; KOB, Z.

Five pion isospin wave functions. Bul Ac Pol mat 11 no. 11:701-706 '63.

1. Institute of Theoretical Physics, University, Warsaw and University Institute for Theoretical Physics, Copenhagen.

KOBA, Z.

On the angular momentum weight factor in the statistical theory of multiple particle production. Pt. 1. Bul Ac Pol nat 9 no.3: 211-216 '61.

1. Institute of Nuclear Research, Polish Academy of Sciences, Warsaw. Presented by L. Infeld.

KOBA, Ziro

On the angular momentum weight factor in the statistical  
theory of multiple particle production. Pt. 2. Bul Ac Pol  
mat 9 no.5:395-401 '61.

1. Institute of Nuclear Research, Polish Academy of Sciences,  
Warsaw. Presented by L. Infeld.



KCHA, Ziro

Statistical theory of multiple particle production with angular momentum conservation. Acta physica Pol 20 no.3:213-234 '61.

1. Institute of Nuclear Research, Polish Academy of Sciences, Warsaw.

33784

P/045/62/021/002/005/007  
B137/B102

24.6700  
AUTHORS:

Koba, Ziro, and Krzywicki, Andrzej

TITLE:

Remarks on the "effective target mass"

PERIODICAL: Acta Physica Polonica, v. 21, no. 2, 1962, 153 - 174

TEXT: The authors investigate the "effective target mass" as defined by N. G. Birger and Yu. A. Smorodin (Zh. eksper. teor. fiz., 37, 1355 (1959)) as to whether or not this experimentally measurable quantity can give certain information on the collision mechanism and the high (some GeV) and superhigh ( $\sim 10^2$  GeV) energy ranges. If an incident particle (nucleon or pion) is assumed to collide, not with the whole target particle (nucleon), but only with a small part of it (e.g., a virtual pion in the cloud) with an effective mass  $m^*$ , this quantity  $m^*$  can be written as  $m^* = \sum_1 (p_{01}^{(1)} - p_1^{(1)} \cos \theta_1^{(1)})$ , where (1) indicates a quantity in the laboratory system, and  $\sum$  denotes summation not including the recoil target nucleon. The invariant quantity  $s^2 = \Delta^2 - \bar{Z}^2 - \Delta_0^2$  plays an

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Remarks on the "effective target ...

essential role in the field-theoretical treatment.  $\vec{\Delta}$  and  $\Delta_0$  denote respectively the energy and momentum transfer between two groups of particles. Since  $\kappa^2$  is not easy to determine experimentally, the authors derive the following relation between  $\kappa$  and  $m^*$ :  $\kappa = m^*/\gamma_s - \sqrt{\gamma_s^2 - 1}$ , where  $\gamma_s$  is the Lorentz factor connecting the so-called S system with the laboratory system. The S-system or minimum-momentum system is characterized by  $\Delta_0(s) = 0$ , i.e., the energy transfer between two groups of particles vanishes. A method for determining  $\kappa$  from measured values of  $m^*$  is given. The effective target mass is examined first within the framework of general kinematic relations which are independent of any interaction mechanism, then from the point of view of the one-pion exchange theory. The ratio of the effective target mass to the whole mass of the target particle is related to partial inelasticity in a system moving in the direction of incidence. A method for determining the mirror inelasticity from the measured recoil momentum is given. A quantum-field theoretical investigation of the target mass on the basis of the one-pion exchange model without and with pole approximation (where the "cross

Card 2/3

KORA, Ziro

Three pion wave functions; method of "effective angular momentum." Acta physica Pol 22:Suppl.:103-125 '62.

1. Institute for Nuclear Research, Warsaw.

S/058/63/000/002/015/070  
A059/A101

AUTHOR: Koba, Ziro

TITLE: Three pion wave functions. Method of "effective angular momentum"

PERIODICAL: Referativnyy zhurnal, Fizika, no. 2, 1963, 17, abstract 2B112  
("Rept. Inst. badań jądrow. PAN", 1962, no. 320/VII, 30 pp, English;  
summaries in Polish and Russian)

TEXT: The system of three pions A, B, and C is examined from the purely kinematic point of view. A method of constructing wave functions in configuration space is suggested, having a given total momentum, total orbital momentum, and parity in the C-system, and prescribed symmetry properties. An assembly of orthonormalized functions is introduced;

$$\begin{aligned} Z_{lm, LM, P, v}(\vec{r}, \vec{r}') &= (p^{1/2}/R^2) Y_l^m(\omega_t) \times \\ &\times Y_L^M(\omega_s) (\sin \theta)^1 (\cos \theta)^L P_v^{(1L)}(\theta) J_{1+L+2v+2}^{(PR)} \end{aligned}$$

where  $s = (1/\sqrt{6})(\vec{r}_A + \vec{r}_B - 2\vec{r}_C)$ ,  $\vec{r} = (1/\sqrt{2})(\vec{r}_A - \vec{r}_B)$ ,  $\omega_s$  and  $\omega_t$  are the solid angles

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Three pion wave functions. Method of...

S/058/63/000/002/015/070  
A059/A101

of vectors  $s$  and  $t$ , respectively,  $\theta = \arctg t/s$ ;  $R^2 = s^2 + t^2$ , and  $p^2 = u^2 + v^2$ , where  $\vec{u}$  and  $\vec{v}$  are momenta canonically conjugated with  $\vec{s}$  and  $\vec{t}$ ;  $P_{\nu}^{(L)}$  are normalized Jacobi polynomials. The new quantum number  $\nu = 0, 1, \dots$  characterizes the distribution of the "total relative momentum"  $P$  between the parts  $u$  and  $v$ ; the less  $\nu$ , the more symmetrical the splitting. The value  $\Lambda = 1 + L + 2\nu$  is denoted as the effective orbital momentum. The states  $\Xi$  with a fixed  $\Lambda$  form a subspace invariant to the group  $S_3$  of permutations of particles  $A, B, C$  between each other. From the wave functions  $\Xi$ , further wave functions with given total momentum, its projection, and  $\Lambda$  are construed, which also form a subspace invariant to transformations of the group  $S_3$ . A table of these functions is presented which correspond to a given irreducible representation of  $S_3$  (with  $\Lambda \leq 4$ ), as well as a table which gives the number of configuration functions with  $\Lambda = 5$  and  $6$ , and a table of isospin functions of three pions. The method can be generalized to a system of four and more pions.

M. Braun

[Abstracter's note: Complete translation]

Card 2/2

GRYNBERG, M.; KOBA, Z.

Four-pion wave functions. *Acta physica Pol* 23 no.4:501-526 Ap '63.

1. Institute for Nuclear Research, Warsaw.

KOBAIDZE, Asen Alekseyevich

[People of Zemo-Kedi on the new road] [Zemokedtay na novom  
puti. Tbilisi, Gos.izd-vo "Sabchota Sakartvelo"] 1963.  
65 p. (MIRA 17:5)



KOBAK, Kira Ivanovna

Some problems concerning the carbon dioxide supply of forest  
biogeocenoses. Problem. skol. i fiziol. les. rast. no.2:61-98  
164.  
(MIRA 18:11)

1. Leningradskaya ordena ienina lesotekhnicheskaya akademiya  
imeni S.M. Kirova.

KOBAK, K.I.

Carbon dioxide concentration in the ground layer of air in  
forest biogeocenoses. Trudy Inst. biol. UPAK SSSR no. 43:  
199-201 '65 (MIRA 19:1)

1. Leningradskaya lesotekhnicheskaya akademiya imeni  
S.M. Kirova.

KOBAL, M.; ANDRIYANOV, P.

Speeding up mechanisation of water supply on livestock farms of  
collective and state farms. Sil'.bud. 10 no.1:3-4 Ja '60.

(MIRA 13:5)

(Ukraine--Water supply, Rural)

AUTHOR: Kobak, V.O.

SOV/106-59-7-6/16

TITLE: Design of "Two-sided" Diode Limiters

PERIODICAL: Elektrosvyaz', 1959, Nr 7, pp 40 - 44 (USSR)

ABSTRACT: Although two-sided diode amplitude limiters, i.e. limiters which clip the top and bottom of signals, find wide application, no detailed analysis has been made from which engineering formulae may be obtained. The author therefore considers four two-sided diode limiter circuits and produces design formulae for them. In the first two circuits, which the author calls "Type A" circuits, the first diode is the lower limiter and the second diode is the upper limiter (Figure 1a). In the second two circuits, Type B, the diode connections are changed round; the first diode is the upper limiter and the second the lower limiter. In the analysis, it is assumed that the internal resistance of the diodes in the conducting direction is constant and equal to  $R_1$ ; in the reverse direction, the resistance is assumed infinite. The static limit thresholds are determined.

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Design of "Two-sided" Diode Limiters

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In a dynamic regime, the results obtained are distorted somewhat, due to inter-electrode capacity. (This problem was investigated in the work of A.Ye. Zhabotinskiy and Yu. L. Svardlov - Ref 1.)

A Type A circuit (which limits positive polarity signals) and its characteristic is shown in Figure 1. For this circuit, the following conditions must hold:

$$E_0 > U_{Bx2} > U_{Bx1} > 0 \quad (1)$$

$$R_1 > R_2 \quad (2)$$

When  $U_{Bx} < U_{Bx1}$  (diode  $\sqrt{1}$  closed) and assuming that:

$$R_1 \ll R, R_1, R_2 \quad (3)$$

then the following relationships are obtained:

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Design of "Two-sided" Diode Limiters

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$$U_{Bx1} \approx U_{Bb1x1} \approx \frac{E_o(a+b)}{a+b+2ab} \quad (4)$$

where

$$a = R_1/R, \quad b = R_2/R.$$

When  $U_{Bx} > U_{Bx2}$  (diode  $\mathcal{J}_2$  closed), then:

$$U_{Bx2} = U_{Bb1x2} \left( c + \frac{c}{a} + 1 \right) - E_o \frac{c}{a} \quad (5)$$

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$$U_{Bb1x2} = \frac{E_o}{1+b} \quad (6)$$

# Design of "Two-sided" Diode Limiters

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where:

$$c = \frac{R_{Bx} + R_1}{R}$$

The symbols are as indicated in Figure 1. For design purposes, these relationships are re-arranged into the forms of Eqs (7) and (8). The value of  $c$  determines the transfer coefficient of the limiter:

$$k = \frac{U_{Bbx2} - U_{Bbx1}}{U_{Bx2} - U_{Bx1}} \quad (10)$$

which can be written as:

$$k = \frac{1}{c \left( \frac{1}{a} + \frac{1}{b} + 2 \right) + 1} \quad (11)$$

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Design of "Two-sided" Diode Limiters

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The procedure for applying these formulae to the computation of the element values is then given. These design formulae can be applied to the reverse diode connection circuit (Figure 3a). Only formula (1) is altered to the form:

$$E_0 < U_{Bx2} < U_{Bx1} < 0.$$

The Type B circuit differs from the Type A in that the first diode limits at the upper level and the second at the lower level. Such a circuit is obtained from the circuit of Figure 3a by changing the negative voltage  $-E_0$  to a positive value  $+E_0$ . This gives greater flexibility since a positive signal can be limited at the upper level and a negative signal at the lower level, depending on the relationship of the elements. Possible characteristics are shown in Figure 4 (I and II). When  $U_{Bx} < U_{Bx1}$ , diode  $\pi_1$  is open and  $\pi_2$  closed. When  $U_{Bx} > U_{Bx2}$ ,

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the converse is true. For normal operation, the following conditions must be fulfilled:

$$E_0 > U_{Bx2} > U_{Bx1},$$

$$E_0 > U_{Bx2} > 0, U_{Bx1} \geq 0 \quad (12)$$

$$R_2 > R_1 \quad (13)$$

The design formulae deduced for this circuit are similar to those for the circuit Type A (Eqs 4-8), except that  $U_{Bx1}$  and  $U_{Bx2}$  are interchanged and also  $U_{Bb1x1}$  and  $U_{Bb1x2}$  are mutually interchanged.

The results of experimental measurements are given in Table 1.

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9.3230 (4140 1153)

AUTHORS: Andreyev, Yu. A., Kobak, V. O.

TITLE: Properties of the double-T bridge, taking into account the effect of the generator and load parameters

PERIODICAL: Elektrosvyaz', no. 7, 1961, 3 - 11

TEXT: All previous publications dealing with the properties of the double-T bridge, and taking into account the generator impedance and the load, are limited to particular cases. The authors of the present article examine the most general case. After a brief recapitulation of the main formulae of the double-T bridge when the generator impedance and the load are not taken into account, the authors present a general analysis of the loaded bridge. The formulae giving the zero-balance condition and the tuning frequency  $\omega_0$  are the same, here, as in the case of the nonloaded bridge. To determine transmission factor T, the author gives the following formula ( $\sigma = \omega/\omega_0$  being the relative detuning, and  $Y = \sigma - 1/\sigma$  the generalized relative detuning):

$$\frac{1}{T} = \frac{U_{\text{inp}}}{U_{\text{outp}}} = (1 - i\frac{D_1}{Y}) + \frac{Z_{\text{gen}}}{Z_T} [(D_1 + D_2) - i\frac{D_1 D_2}{Y}] - i\frac{Z_T}{Z_1} \frac{1}{Y} + \frac{Z_{\text{gen}}}{Z_1} (1 - i\frac{D_2}{Y}) \quad (5)$$

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where:

$$Z_T = R_1 \left( \frac{1+\beta}{\sqrt{\alpha\beta n}} - 1 \right) \frac{(1+\alpha)}{\alpha}$$

$$D_1 = \frac{\alpha(1+\beta) + \beta n(1+\alpha)}{\sqrt{\alpha\beta n}}$$

$$D_2 = \frac{(1+\beta) + n(1+\alpha)}{\sqrt{\alpha\beta n}}$$

n being any positive number ( $0 < n < \infty$ ),  $\alpha = R_1/R_2$  and  $\beta = C_2/C_1$ . The balance conditions of the bridge characteristics are determined, in the general case, by the relations

$$\begin{aligned} \operatorname{Re} T(\omega) &= \operatorname{Re} T\left(\frac{1}{\omega}\right) \\ \operatorname{Im} T(\omega) &= -\operatorname{Im} T\left(\frac{1}{\omega}\right) \end{aligned} \quad (6)$$

The analysis of the possible ways of connecting the double-T bridges reveals that, from the point of view of their use in selective tube (or transistorized) amplifiers, the most interesting connection is that shown in Fig. 4. In this case,  $C_{\text{gen}}$  represents the transfer capacitance from the anode of a tube,  $R_{\text{gen}}$  is determined by the anode load and the internal tube resistance,  $R_1$  is the input resistance of

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a tube, and  $C_1$  serves only to balance the bridge characteristics. The authors analyze the conditions (relating the parameters of the generator, of the load and of the bridge) to be satisfied for the symmetry of the amplitude-phase characteristics of the circuit of Fig. 4. There are five variants of these conditions. The most interesting connection is:

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$$R_1 C_1 = n R_{\text{gen}} C_{\text{gen}}; \quad R_1 C_1 = R_1 C_1; \quad R_1 C_1 = R_2 C_2; \quad R_1 R_2 = (1+n) R_{\text{gen}} R_1 \quad (8d)$$

The transmission factor is given by the following expression, whichever of the five sets of conditions is satisfied:

$$T = \frac{T_m}{1 - \frac{d_1}{Y} + i \frac{Y}{d_2}} \quad (9)$$

In the case of conditions (8d):

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$$\left. \begin{aligned} T_m &= \frac{\alpha^2}{(\alpha+\delta)(\alpha+\delta+2\alpha\delta)} \\ d_1 &= \frac{(1+n)(1+\alpha)(\alpha+\delta)^2}{\sqrt{n\alpha}} T_m \\ d_2 &= \frac{(1+n)\alpha}{\delta^2 \sqrt{n\alpha}} \end{aligned} \right\} \quad (10)$$

where  $\delta = \frac{R_1}{R_2}$ ,  $\alpha = \frac{R_1}{R_2}$ . The frequency characteristic of the bridge, in the general case examined by the author, is

$$|T| = \frac{T_m}{\sqrt{1 + \left(\frac{d_1}{Y} - \frac{Y}{d_2}\right)^2}} \quad (11)$$

The phase characteristics are calculated according to formula:

$$\varphi = \arctan \left( \frac{d_1}{Y} - \frac{Y}{d_2} \right).$$

Using (9), it is easy to plot the amplitude-phase characteristic of the bridge in the complex plane. This characteristic consists of two superposed circumferences. The Q-factor of an RC selective system is determined, in the general case, as the

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steepness of the frequency characteristic at the tuning frequency. As applied to the case of formula (9), the Q-factor is:

$$Q = \frac{d \left| \frac{T}{T_m} \right|}{dY} \Big|_{Y=0} = \frac{1}{d_1}. \quad (12)$$

After examining several particular cases (for instance, the case of a symmetrical bridge system  $R_1 = R_2 = R$ ,  $C_1 = C_2 = C$ ), the authors draw the following conclusions as to the properties of the double-T bridge, considering the effect of generator and load parameters. 1) The double-T bridge (in real systems) possesses symmetrical amplitude-phase characteristics only when a definite relationship exists between the parameters of the generator, of the load and of the bridge. 2) Symmetrical characteristics of the bridge are obtained only if the load and the generator internal impedance are both either purely resistive or purely capacitive, or when they are both resistive-capacitive. Any mixed case leads to unavoidable asymmetry. 3) The selectivity of a selective amplifier with a double-T bridge is much worse, at a great detuning, than it was generally supposed. There are 7 figures and 7 references: 4 Soviet-bloc and 3 non-Soviet-bloc. The references to English-language publications read as follows: Cowles, The parallel - T resistance-capacitance network. Proc.IRE, 1952, no. 12; Buckley, Parallel-T network. "Wireless Engineer".

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Properties of the double-T bridge...

1956, no. 7; Yosiro Oono, Design of parallel-T resistance-capacitance network. Proc.IRE, 1955, no. 5.

SUBMITTED: December 12, 1960

[Abstracter's note: The following subscripts are translated in the text and formulae: l (load) stands for H; gen (generator) stands for r or l.]

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Kobakhidze, A. G. - "The theory for the reduction of manganese oxides to  $MnO$ ," A commemorative collection of transactions dedicated to the 25th anniversary of the Institute, (Gruz. politekh. in-t im. Kirova, No 17), Tbilisi, 1948, p. 431-43, (Resume in Georgian)

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ANDREYEV, Yu.A.; KOBAK, V.O.

Features of a double T-shaped bridge with consideration to the  
effects of the parameters of the generator and load. *Elektrosvyaz'*  
15 no.7:3-11 J1 '61. (MIRA 14:6)  
(Bridge circuits) (Electric networks)

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8/106/62/000/002/002/001  
A055/A101

9.3240 (1040, 1139, 1154)  
Kobak, V.O.

AUTHOR:

TITLE:

PERIODICAL: *Elektrosvyaz*, no. 2, 1962, 10 - 16  
Possibilities offered by amplifiers with negative feedback through a double T-bridge

TEXT:

This article is a comparative estimate of the possibilities offered by various selective amplifier systems with negative feedback through a double T-bridge. The effect of the generator and load parameters on the properties of the bridge are not taken into account. The amplifier without feedback is assumed to be linear and having a purely real and frequency-independent amplification factor  $K_0 > 1$ . Since only negative feedback is considered, a negative amplification factor  $-|K_0| = -K_0$  is introduced. The following assumptions are also made: 1) The input impedance of the amplifier  $Z_{inp}$  is great, and its output impedance  $Z_{outp}$  is small. 2) The passive "three-pole" quadripole in the feedback circuit has a complex transmission coefficient  $T$ , and its input and output impedances ( $Z_1$  and  $Z_2$ , respectively) satisfy the inequalities:  $|Z_{outp}| < |Z_1|$ ,  $|Z_2| < |Z_{inp}|$ . 3) The input signal source  $E$  has a zero internal impedance. Under all these assumptions,

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the author examines five possible ways of inserting  $E$  into the amplifier circuit (Fig. 1) and determines the overall amplification factor for different combinations of  $E$  and of the output voltage  $U$ , i.e., he determines:

$$K_1 = U_n/E_m \text{ at } \begin{cases} n = 1, 2, 3, 4, 5 \\ m = 1, 2, 3, 4. \end{cases}$$

Eight formulae (giving  $K_1, K_2, \dots, K_8$  for each of these eight combinations, respectively) are thus obtained. The author passes next to the case when a double T-bridge is used as the "three-pole" in the feedback circuit. He deduces six formulae giving, in this case, the scalar amplification factor for the first six combinations, i.e.,  $|K_1|$  to  $|K_6|$ , and discusses these formulae. He also calculates the scalar amplification factor  $|K_9|$  for a special case, when  $E$  is inserted into the "middle" of the amplifier, as shown in Figure 5. At the end of the article, the author reproduces the diagrams of four of the most interesting practical realizations of one-stage selective amplifiers with a double T-bridge in the feedback circuit, and briefly discusses these diagrams. There are 6 figures, and 9 references: 7 Soviet-bloc and 2 non-Soviet-bloc. The English-language reference reads as follows: Ward, Landshoff, Parallel - T RC selective amplifiers. *Electronic and Radio Engineer*, v. 35, no. 4, 1958. The Soviet authors and scientists mentioned in the article are: L.S. Gutkin, Yu.G. Kochinev, R.Ya. Berkman, Yu.I.

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ANDREYEV, Yuriy Aleksandrovich; KOBAK, Valeriy Oskarovich;  
MICHURIN, V.I., kand. tekhn. nauk, retsenzent; APTEKMAN,  
M.A., red.; TSAL, R.K., tekhn. red.

[Double T-shaped bridges in selective amplifiers] Dvoynye  
T-obraznye mosty v isbiratel'nykh usiliteliakh. Leningrad,  
Sudpromgiz, 1962. 103 p. (MIRA 15:9)  
(Amplifiers, Electron-tube) (Bridge circuits)

Doppler effect: the ...  
(Microwave Journal, 1960, no. 11), by C. G. Bachman et al. (Microwave Journal,

Card 1/2 APPROVED FOR RELEASE: 09/18/2001 UDC: 621.372.6.01  
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ACC NR: AP7004340

1963, nos. 2-3), and by other researchers. The model performs a reciprocating (sinusoidal-law) motion along the signal-transmission line. The required tuning

frequency can be determined from this formula:  $T = \frac{4\pi S_0}{F_{0.7} \lambda \sqrt{2}}$ ; the required pass-

band of the receiving channel is:  $\Delta F_{0.7} > 2 \sqrt{\frac{\pi F_0}{T}} = F_0 \sqrt{\frac{1.41 \lambda}{S_0}}$ . Here: T -

reciprocating-motion period;  $S_0$  - motion amplitude;  $F_{0.7}$  - amplifier resonance frequency;  $Q_0 = F_0 / \Delta F_{0.7}$  - equivalent Q-factor of the frequency-selective amplifier;  $\lambda$  - wavelength. A numerical example illustrates the use of the above approximate formulas. Orig. art. has: 2 figures and 10 formulas.

SUB CODE: 09 / SUBM DATE: none / ORIG REF: 005 / OTH REF: 003

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